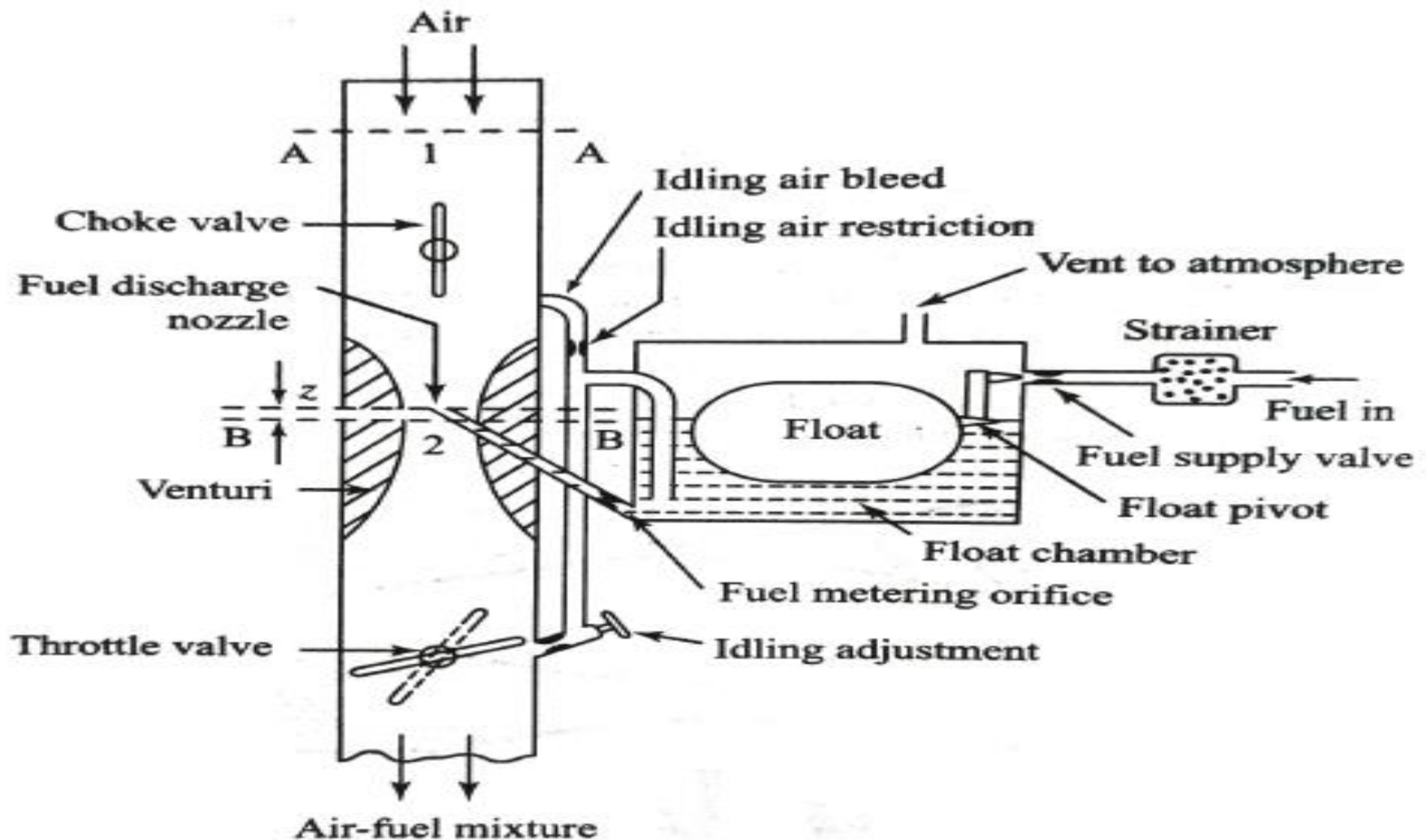


Calculation of Air Fuel Ratio



Applying the steady flow energy equation to sections AA and B-B and assuming unit mass flow of air, we have,

$$q - w = (h_2 - h_1) + \frac{1}{2}(C_2^2 - C_1^2)$$

Here q , w are the heat and work transfers from entrance to throat and h and C stand for enthalpy and velocity respectively.

Assuming an adiabatic flow, we get $q = 0$, $w = 0$ and $C_1 \approx 0$,

$$C_2 = \sqrt{2(h_1 - h_2)}$$

Assuming air to behave like ideal gas, we get $h = C_p T$. Hence, written as,

$$C_2 = \sqrt{2C_p(T_1 - T_2)}$$

As the flow process from inlet to the venturi throat can be considered to be isentropic, we have

$$\frac{T_2}{T_1} = \left(\frac{p_2}{p_1}\right)^{\left(\frac{\gamma-1}{\gamma}\right)}$$

$$T_1 - T_2 = T_1 \left[1 - \left(\frac{p_2}{p_1}\right)^{\left(\frac{\gamma-1}{\gamma}\right)}\right]$$

Substituting Eq.7.5 in Eq.7.3, we get

$$C_2 = \sqrt{2C_p T_1 \left[1 - \left(\frac{p_2}{p_1}\right)^{\left(\frac{\gamma-1}{\gamma}\right)}\right]}$$

Now, mass flow of air,

$$\dot{m}_a = \rho_1 A_1 C_1 = \rho_2 A_2 C_2$$

where A_1 and A_2 are the cross-sectional area at the air inlet (point 1) and venturi throat (point 2).

To calculate the mass flow rate of air at venturi throat, we have

$$p_1/\rho_1^\gamma = p_2/\rho_2^\gamma$$

$$\rho_2 = (p_2/p_1)^{1/\gamma} \rho_1$$

$$\dot{m}_a = \left(\frac{p_2}{p_1}\right)^{1/\gamma} \rho_1 A_2 \sqrt{2C_p T_1 \left[\left(1 - \frac{p_2}{p_1}\right)^{\frac{\gamma-1}{\gamma}} \right]}$$

$$= \left(\frac{p_2}{p_1}\right)^{1/\gamma} \frac{p_1}{RT_1} A_2 \sqrt{2C_p T_1 \left[1 - \left(\frac{p_2}{p_1}\right)^{\frac{\gamma-1}{\gamma}} \right]}$$

$$= \frac{A_2 p_1}{R \sqrt{T_1}} \sqrt{2C_p \left[\left(\frac{p_2}{p_1} \right)^{\frac{2}{\gamma}} - \left(\frac{p_2}{p_1} \right)^{\frac{\gamma+1}{\gamma}} \right]}$$

Substituting $C_p = 1005 \text{ J/kg K}$, $\gamma = 1.4$ and $R = 287 \text{ J/kg K}$ for air,

$$\begin{aligned} \dot{m}_a &= 0.1562 \frac{A_2 p_1}{\sqrt{T_1}} \sqrt{\left(\frac{p_2}{p_1} \right)^{1.43} - \left(\frac{p_2}{p_1} \right)^{1.71}} \\ &= 0.1562 \frac{A_2 p_1}{\sqrt{T_1}} \phi \text{ kg/s} \end{aligned}$$

where

$$\phi = \sqrt{\left(\frac{p_2}{p_1} \right)^{1.43} - \left(\frac{p_2}{p_1} \right)^{1.71}}$$

Here, p is in N/m^2 , A is in m^2 and T is in K .

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To get the actual mass flow rate, the above equation should be multiplied by the co-efficient of discharge for the venturi, C_{da} .

$$\dot{m}_{\text{actual}} = 0.1562 C_{da} \frac{A_2 p_1}{\sqrt{T_1}} \phi$$

Since C_{da} and A_2 are constants for a given venturi,

$$\dot{m}_{\text{actual}} \propto \frac{p_1}{\sqrt{T_1}} \phi$$

In order to calculate the air-fuel ratio, fuel flow rate is to be calculated. As the fuel is incompressible, applying Bernoulli's Theorem we get

$$\frac{p_1}{\rho_f} - \frac{p_2}{\rho_f} = \frac{C_f^2}{2} + gz$$

where ρ_f is the density of fuel, C_f is the fuel velocity at the nozzle exit and z is the height of the nozzle exit above the level of fuel in the float bowl

$$C_f = \sqrt{2 \left[\frac{p_1 - p_2}{\rho_f} - gz \right]}$$

Mass flow rate of fuel,

$$\begin{aligned} \dot{m}_f &= A_f C_f \rho_f \\ &= A_f \sqrt{2 \rho_f (p_1 - p_2 - gz \rho_f)} \end{aligned}$$

where A_f is the area of cross-section of the nozzle and ρ_f is the density of the fuel

$$\dot{m}_{f_{actual}} = C_{df} A_f \sqrt{2\rho_f (p_1 - p_2 - gz\rho_f)}$$

where C_{df} is the coefficient of discharge for fuel nozzle

$$A/F \text{ ratio} = \frac{\dot{m}_{a_{actual}}}{\dot{m}_{f_{actual}}}$$

$$\frac{A}{F} = 0.1562 \frac{C_{da} A_2}{C_{df} A_f} \frac{p_1 \phi}{\sqrt{2T_1 \rho_f (p_1 - p_2 - gz\rho_f)}}$$