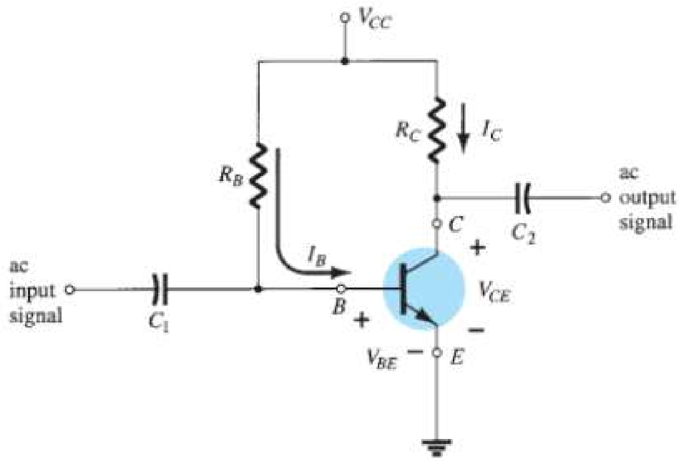
- Fixed-Bias Configuration
- Emitter-Bias Configuration
- Voltage-Divider Bias Configuration
- Collector Feedback Configuration
- Emitter-Follower Configuration
- Common-Base Configuration
- Miscellaneous Bias Configurations

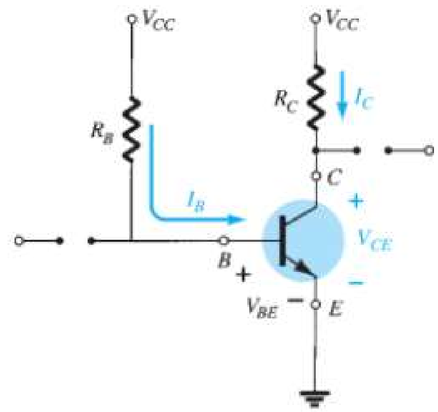
TRANSISTOR DC BIAS CONFIGURATIONS

Fixed-Bias Configuration

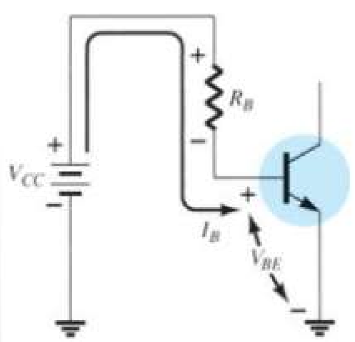
- Fixed-bias circuit.



- DC equivalent ct.



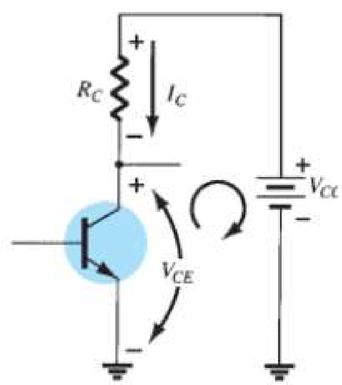
- Base–emitter loop.



$$+V_{CC} - I_B R_B - V_{BE} = 0$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B}$$

- Collector–emitter loop.



$$I_C = \beta I_B$$

$$V_{CE} + I_C R_C - V_{CC} = 0$$

$$V_{CE} = V_{CC} - I_C R_C$$

$$V_{CE} = V_C - V_E$$

$$V_{CE} = V_C$$

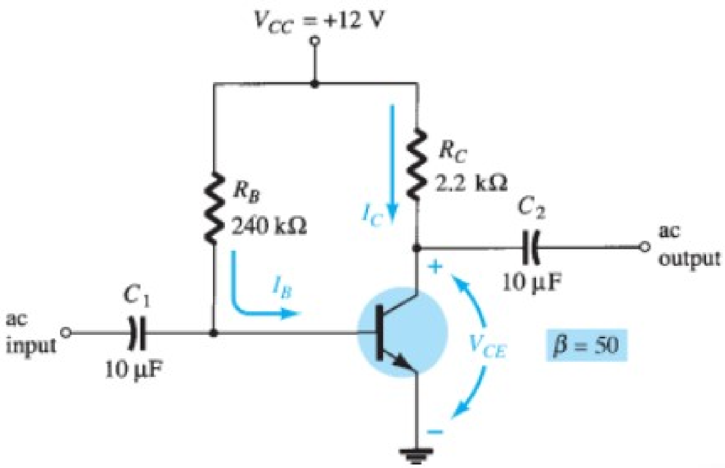
$$V_{BE} = V_B - V_E$$

$$V_{BE} = V_B$$

Fixed-Bias Configuration Example

EXAMPLE 4.1 Determine the following for the fixed-bias configuration

a. I_{B_Q} and I_{C_Q}.
b. V_{CE_Q}.
c. V_B and V_C.
d. V_{BC}.



Solution:

a. Eq. (4.4): $I_{B_Q} = \dfrac{V_{CC} - V_{BE}}{R_B} = \dfrac{12\text{ V} - 0.7\text{ V}}{240\text{ k}\Omega} = \mathbf{47.08\ \mu A}$

Eq. (4.5): $I_{C_Q} = \beta I_{BQ} = (50)(47.08\ \mu\text{A}) = \mathbf{2.35\ mA}$

b. Eq. (4.6):
$$\begin{aligned} V_{CE_Q} &= V_{CC} - I_C R_C \\ &= 12\text{ V} - (2.35\text{ mA})(2.2\text{ k}\Omega) \\ &= \mathbf{6.83\ V} \end{aligned}$$

c. $V_B = V_{BE} = \mathbf{0.7\ V}$
$V_C = V_{CE} = \mathbf{6.83\ V}$

d. Using double-subscript notation yields

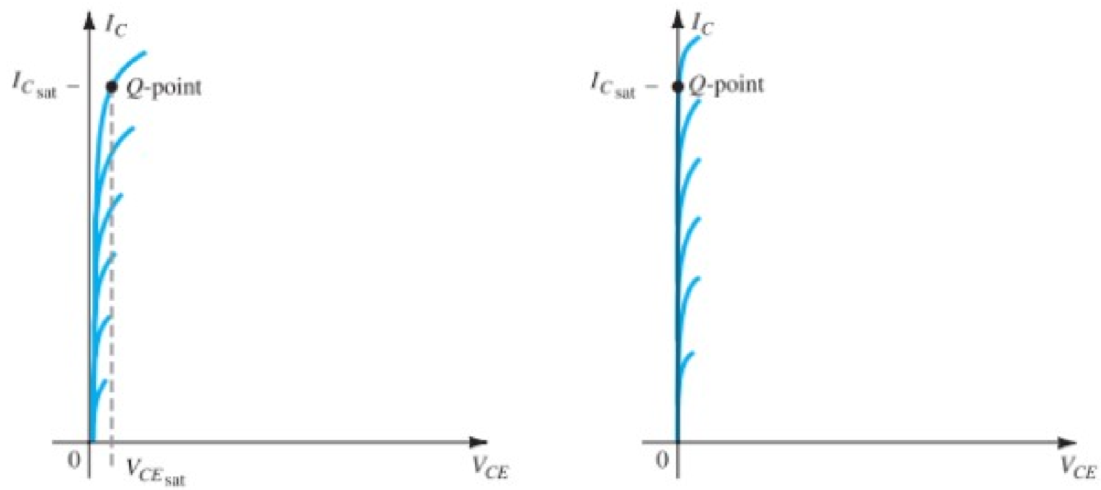
$$\begin{aligned} V_{BC} &= V_B - V_C = 0.7\text{ V} - 6.83\text{ V} \\ &= \mathbf{-6.13\ V} \end{aligned}$$

with the negative sign revealing that the junction is reversed-biased, as it should be for linear amplification.

Fixed-Bias Configuration …

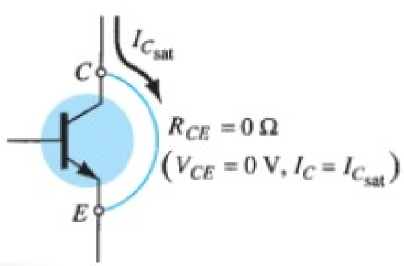
- **Transistor Saturation**

- Saturation regions:
  (a) Actual
  (b) approximate.



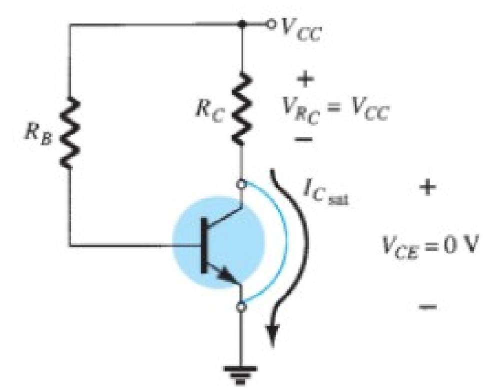
(a) (b)

- Determining I_{Csat}



$$R_{CE} = \frac{V_{CE}}{I_C} = \frac{0\text{ V}}{I_{C_{sat}}} = 0\,\Omega$$

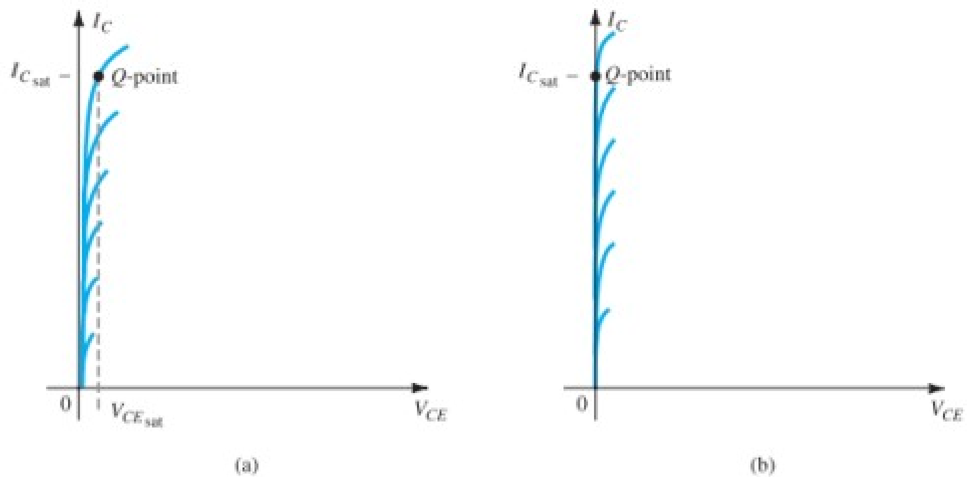
- Determining I_{Csat} for the fixed-bias configuration.



$$I_{C_{sat}} = \frac{V_{CC}}{R_C}$$

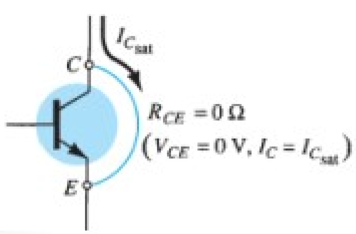
Fixed-Bias Configuration ...

- **Transistor Saturation**



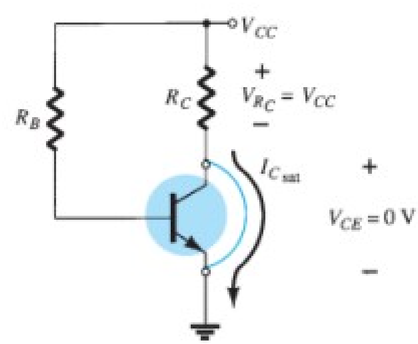
- Saturation regions:
  (a) Actual
  (b) approximate.

- Determining I_{Csat}



$$R_{CE} = \frac{V_{CE}}{I_C} = \frac{0\ V}{I_{C_{sat}}} = 0\ \Omega$$

- Determining I_{Csat} for the fixed-bias configuration.



$$I_{C_{sat}} = \frac{V_{CC}}{R_C}$$

Fixed-Bias Configuration …

- **Load Line Analysis**

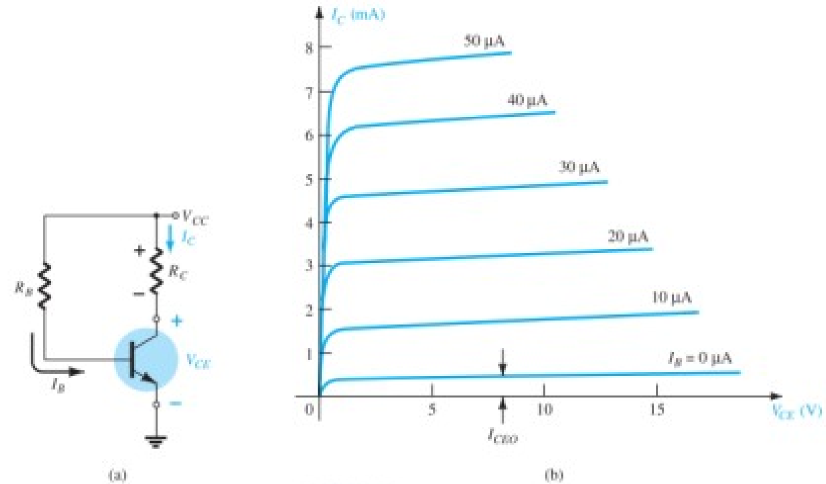
$$V_{CE} = V_{CC} - I_C R_C$$

$$V_{CE} = V_{CC} - (0)R_C$$

$$V_{CE} = V_{CC}\big|_{I_C = 0\,\mathrm{mA}}$$

$$0 = V_{CC} - I_C R_C$$

$$I_C = \frac{V_{CC}}{R_C}\bigg|_{V_{CE}=0\,\mathrm{V}}$$



Load-line analysis: (a) the network; (b) the device characteristics.

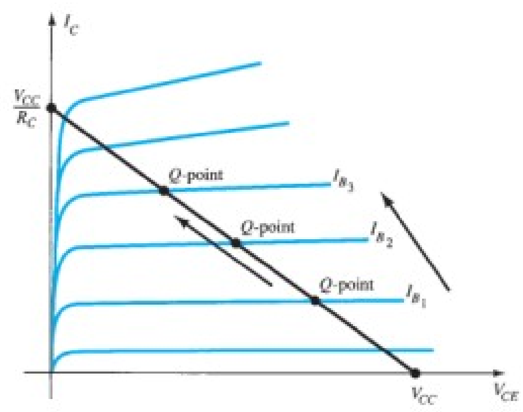


FIG. 4.13
Movement of the Q-point with increasing level of I_B.

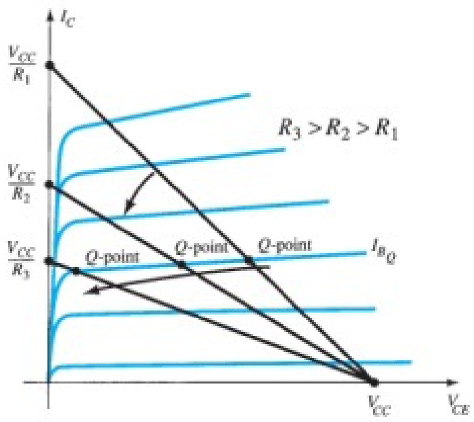


FIG. 4.14
Effect of an increasing level of R_C on the load line and the Q-point.

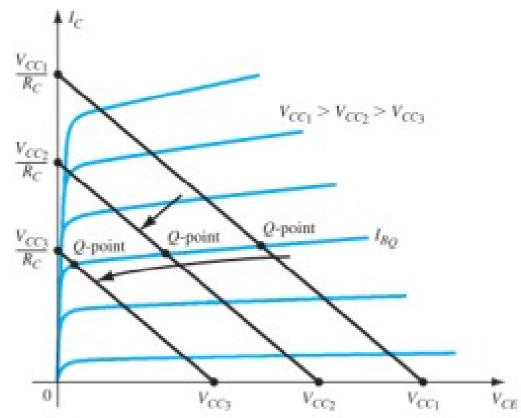
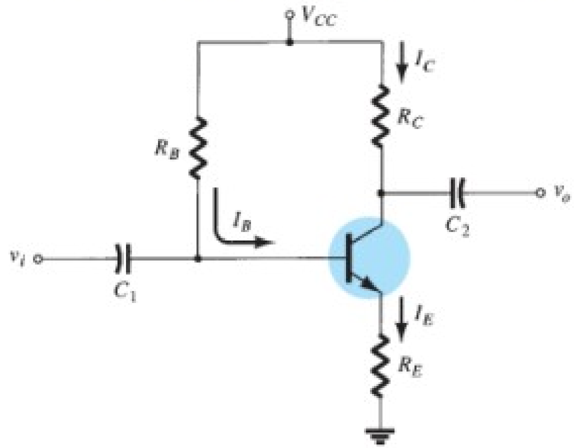


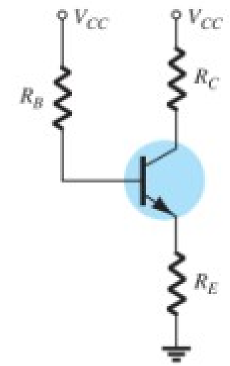
FIG. 4.15
Effect of lower values of V_{CC} on the load line and the Q-point.

Emitter-Bias Configuration

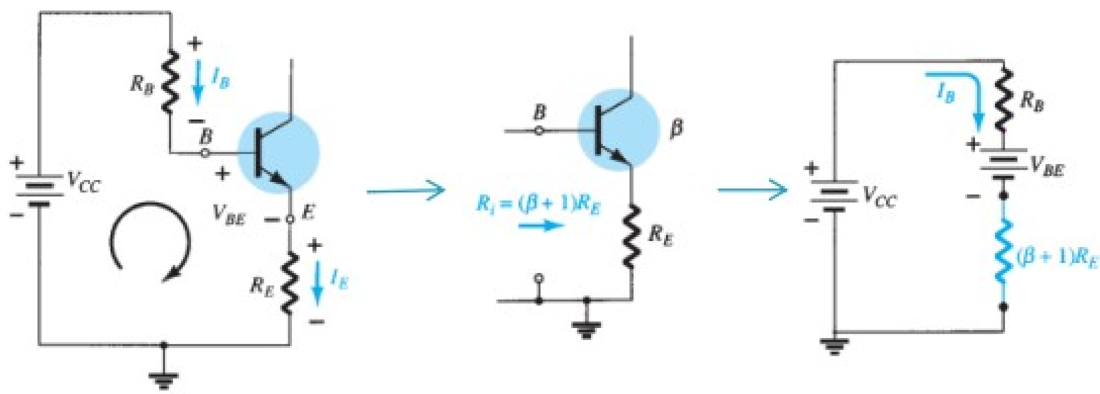
- BJT bias circuit with emitter resistor.



- DC equivalent ct



- Base-Emitter Loop



$$+V_{CC} - I_B R_B - V_{BE} - I_E R_E = 0$$

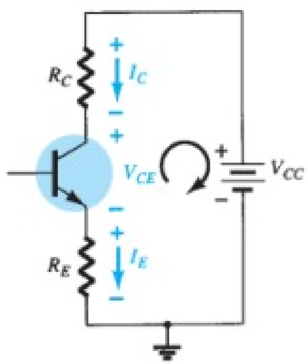
$$I_E = (\beta + 1) I_B$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E}$$

$$R_i = (\beta + 1)R_E$$

Emitter-Bias Configuration

Collector-Emitter Loop



$$+I_E R_E + V_{CE} + I_C R_C - V_{CC} = 0$$

$$I_E \cong I_C$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

$$V_E = I_E R_E$$

$$V_{CE} = V_C - V_E$$

$$V_C = V_{CE} + V_E$$

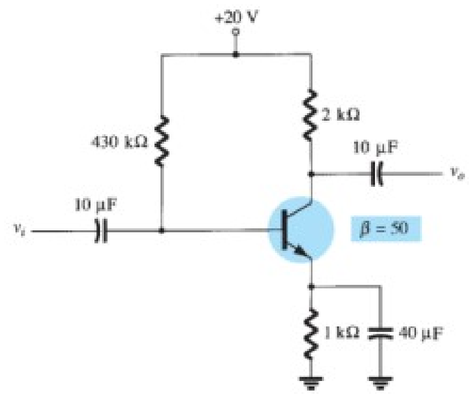
$$V_B = V_{CC} - I_B R_B$$

$$V_C = V_{CC} - I_C R_C$$

$$V_B = V_{BE} + V_E$$

EXAMPLE 4.4 For the emitter-bias network of Fig. 4.23, determine:

a. I_B.
b. I_C.
c. V_{CE}.
d. V_C.
e. V_E.
f. V_B.
g. V_{BC}.



Solution:

a. Eq. (4.17): $I_B = \dfrac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E} = \dfrac{20\text{ V} - 0.7\text{ V}}{430\text{ k}\Omega + (51)(1\text{ k}\Omega)}$

$= \dfrac{19.3\text{ V}}{481\text{ k}\Omega} = \mathbf{40.1\ \mu A}$

b. $I_C = \beta I_B$

$= (50)(40.1\ \mu\text{A})$

$\cong \mathbf{2.01\ mA}$

c. Eq. (4.19): $V_{CE} = V_{CC} - I_C(R_C + R_E)$

$= 20\text{ V} - (2.01\text{ mA})(2\text{ k}\Omega + 1\text{ k}\Omega) = 20\text{ V} - 6.03\text{ V}$

$= \mathbf{13.97\ V}$

d. $V_C = V_{CC} - I_C R_C$

$= 20\text{ V} - (2.01\text{ mA})(2\text{ k}\Omega) = 20\text{ V} - 4.02\text{ V}$

$= \mathbf{15.98\ V}$

e. $V_E = V_C - V_{CE}$

$= 15.98\text{ V} - 13.97\text{ V}$

$= \mathbf{2.01\ V}$

or $V_E = I_E R_E \cong I_C R_E$

$= (2.01\text{ mA})(1\text{ k}\Omega)$

$= \mathbf{2.01\ V}$

f. $V_B = V_{BE} + V_E$

$= 0.7\text{ V} + 2.01\text{ V}$

$= \mathbf{2.71\ V}$

g. $V_{BC} = V_B - V_C$

$= 2.71\text{ V} - 15.98\text{ V}$

$= \mathbf{-13.27\ V}$ (reverse-biased as required)

Emitter-Bias Configuration

- Improved bias stability (check example 4.5)

The addition of the emitter resistor to the dc bias of the BJT provides improved stability, that is, the dc bias currents and voltages remain closer to where they were set by the circuit when outside conditions, such as temperature and transistor beta, change.

Effect of β variation on the response of the fixed-bias configuration of Fig. 4.7.

β	I_B (μA)	I_C (mA)	V_{CE} (V)
50	47.08	2.35	6.83
100	47.08	4.71	1.64

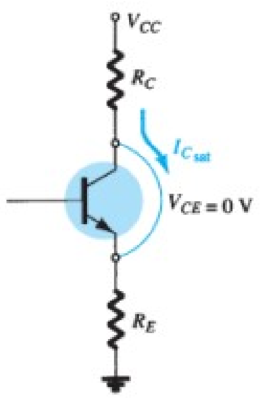
The BJT collector current is seen to change by 100% due to the 100% chan of β. The value of I_B is the same, and V_{CE} decreased by 76%.

Effect of β variation on the response of the emitter-bias configuration of Fig. 4.23.

β	I_B (μA)	I_C (mA)	V_{CE} (V)
50	40.1	2.01	13.97
100	36.3	3.63	9.11

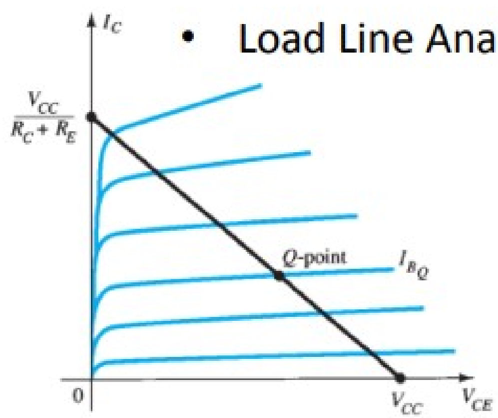
Now the BJT collector current increases by about 81% due to the 100% increase in β. Notice that I_B decreased, helping maintain the value of I_C—or at least reducing the overall change in I_C due to the change in β. The change in V_{CE} has dropped to about 35%. The network of Fig. 4.23 is therefore more stable than that of Fig. 4.7 for the same change in β.

- Saturation Level



$$I_{C_{sat}} = \frac{V_{CC}}{R_C + R_E}$$

- Load Line Analysis

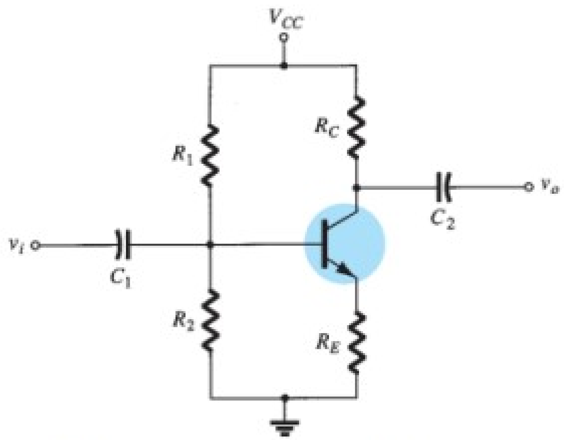


$$V_{CE} = V_{CC}\big|_{I_C = 0\,\text{mA}}$$

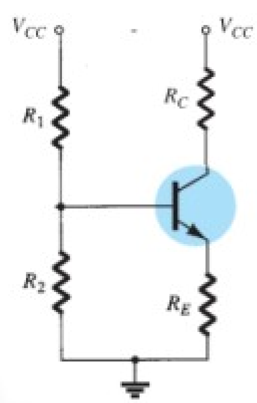
$$I_C = \frac{V_{CC}}{R_C + R_E}\Bigg|_{V_{CE} = 0\,\text{V}}$$

Voltage-Divider Configuration

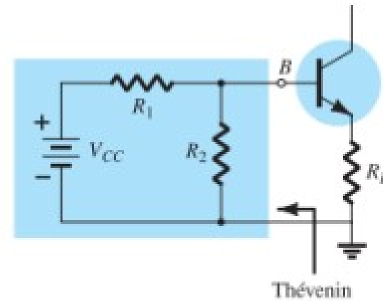
- Voltage-divider bias configuration.

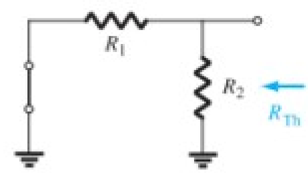


- DC components of the voltage-divider configuration.

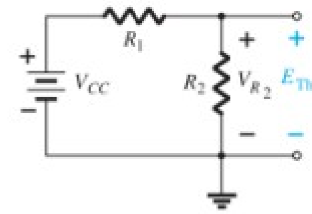


- Exact Analysis

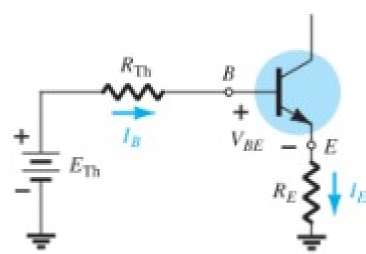




$$R_{Th} = R_1 \| R_2$$



$$E_{Th} = V_{R_2} = \frac{R_2 V_{CC}}{R_1 + R_2}$$

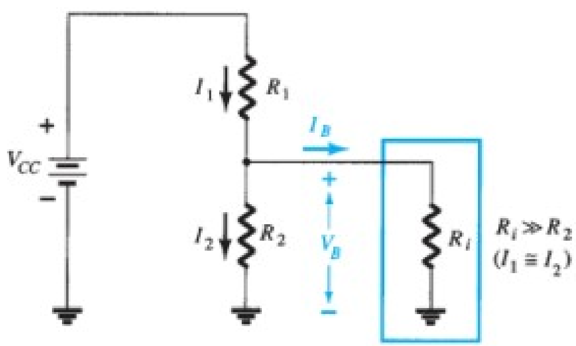


$$I_B = \frac{E_{Th} - V_{BE}}{R_{Th} + (\beta + 1)R_E}$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

Voltage-Divider Configuration

- Approximate Analysis



$$V_B = \frac{R_2 V_{CC}}{R_1 + R_2}$$

$$R_i = (\beta + 1)R_E \cong \beta R_E$$

$$\beta R_E \geq 10 R_2$$

$$V_E = V_B - V_{BE}$$

$$I_E = \frac{V_E}{R_E}$$

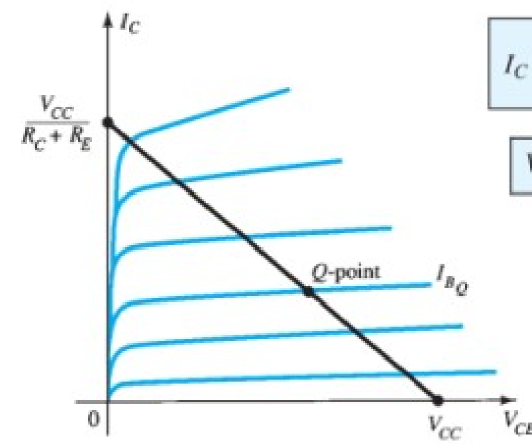
$$I_{C_Q} \cong I_E$$

$$V_{CE_Q} = V_{CC} - I_C(R_C + R_E)$$

- Transistor Saturation

$$I_{C_{sat}} = I_{C_{max}} = \frac{V_{CC}}{R_C + R_E}$$

- Load-Line Analysis



$$I_C = \left.\frac{V_{CC}}{R_C + R_E}\right|_{V_{CE} = 0\text{ V}}$$

$$V_{CE} = V_{CC}\big|_{I_C = 0\text{ mA}}$$

Voltage-Divider Configuration Example

EXAMPLE 4.11 Determine the levels of I_{C_Q} and V_{CE_Q} for the voltage-divider configuration of Fig. 4.37 using the exact and approximate techniques and compare solutions. In this case, the conditions of Eq. (4.33) *will not be satisfied* and the results will reveal the difference in solution if the criterion of Eq. (4.33) is ignored.

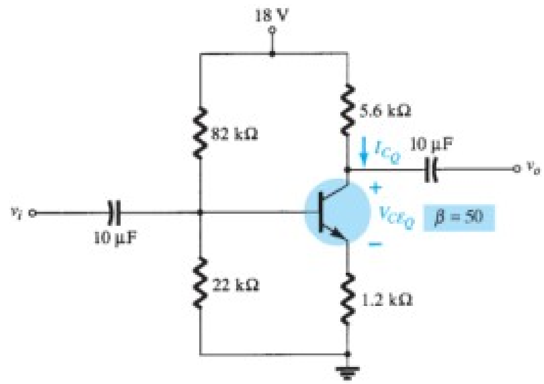


FIG. 4.37
Voltage-divider configuration for Example 4.11.

Solution: Exact analysis:

Eq. (4.33):

$$\beta R_E \geq 10R_2$$
$$(50)(1.2\,\text{k}\Omega) \geq 10(22\,\text{k}\Omega)$$
$$60\,\text{k}\Omega \ngeq 220\,\text{k}\Omega \text{ (not satisfied)}$$
$$R_{\text{Th}} = R_1 \| R_2 = 82\,\text{k}\Omega \| 22\,\text{k}\Omega = 17.35\,\text{k}\Omega$$
$$E_{\text{Th}} = \frac{R_2 V_{CC}}{R_1 + R_2} = \frac{22\,\text{k}\Omega(18\text{ V})}{82\,\text{k}\Omega + 22\,\text{k}\Omega} = 3.81\text{ V}$$
$$I_B = \frac{E_{\text{Th}} - V_{BE}}{R_{\text{Th}} + (\beta + 1)R_E} = \frac{3.81\text{ V} - 0.7\text{ V}}{17.35\,\text{k}\Omega + (51)(1.2\,\text{k}\Omega)} = \frac{3.11\text{ V}}{78.55\,\text{k}\Omega} = 39.6\,\mu\text{A}$$
$$I_{C_Q} = \beta I_B = (50)(39.6\,\mu\text{A}) = \mathbf{1.98\,mA}$$
$$V_{CE_Q} = V_{CC} - I_C(R_C + R_E)$$
$$= 18\text{ V} - (1.98\text{ mA})(5.6\,\text{k}\Omega + 1.2\,\text{k}\Omega)$$
$$= \mathbf{4.54\,V}$$

Approximate analysis:

$$V_B = E_{\text{Th}} = 3.81\text{ V}$$
$$V_E = V_B - V_{BE} = 3.81\text{ V} - 0.7\text{ V} = 3.11\text{ V}$$
$$I_{C_Q} \cong I_E = \frac{V_E}{R_E} = \frac{3.11\text{ V}}{1.2\,\text{k}\Omega} = \mathbf{2.59\,mA}$$
$$V_{CE_Q} = V_{CC} - I_C(R_C + R_E)$$
$$= 18\text{ V} - (2.59\text{ mA})(5.6\,\text{k}\Omega + 1.2\,\text{k}\Omega)$$
$$= \mathbf{3.88\,V}$$

Comparing the exact and approximate approaches.

	I_{C_Q} (mA)	V_{CE_Q} (V)
Exact	1.98	4.54
Approximate	2.59	3.88

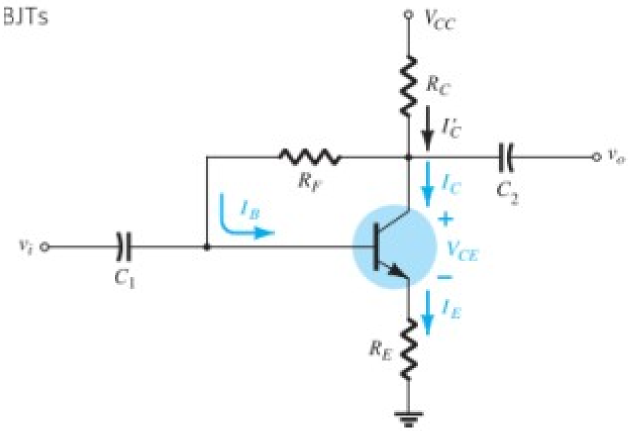
The results reveal the difference between exact and approximate solutions. I_{C_Q} is about 30% greater with the approximate solution, whereas V_{CE_Q} is about 10% less. The results are notably different in magnitude, but even though βR_E is only about three times larger than R_2, the results are still relatively close to each other. For the future, however, our analysis will be dictated by Eq. (4.33) to ensure a close similarity between exact and approximate solutions.

$$\boxed{\beta R_E \geq 10R_2} \quad \textbf{(4.33)}$$

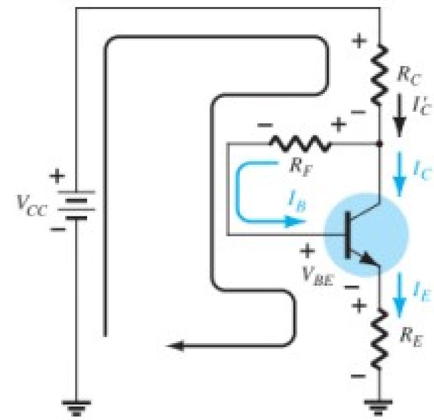
Collector Feedback Configuration

- DC bias circuit with voltage feedback.

BJTs



- Base–Emitter Loop



$$V_{CC} - V_{BE} - \beta I_B(R_C + R_E) - I_B R_F = 0$$

$$I_B = \frac{V_{CC} - V_{BE}}{R_F + \beta(R_C + R_E)}$$

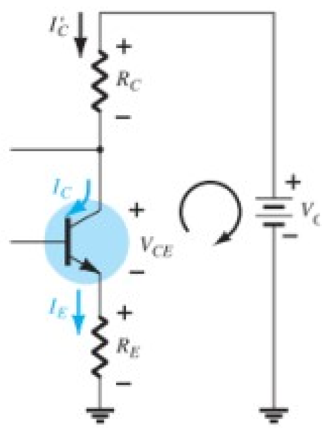
$$I_B = \frac{V'}{R_F + \beta R'}$$

$$R' = R_E.$$

$$I_{C_Q} = \frac{\beta V'}{R_F + \beta R'} = \frac{V'}{\frac{R_F}{\beta} + R'}$$

$$I_{C_Q} \cong \frac{V'}{R'}$$

- Collector–Emitter Loop



$$I_E R_E + V_{CE} + I_C' R_C - V_{CC} = 0$$

Because $I_C' \cong I_C$ and $I_E \cong I_C$, we have

$$I_C(R_C + R_E) + V_{CE} - V_{CC} = 0$$

and

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

Collector Feedback Configuration

- Saturation Conditions

Using the approximation $I'_C = I_C$

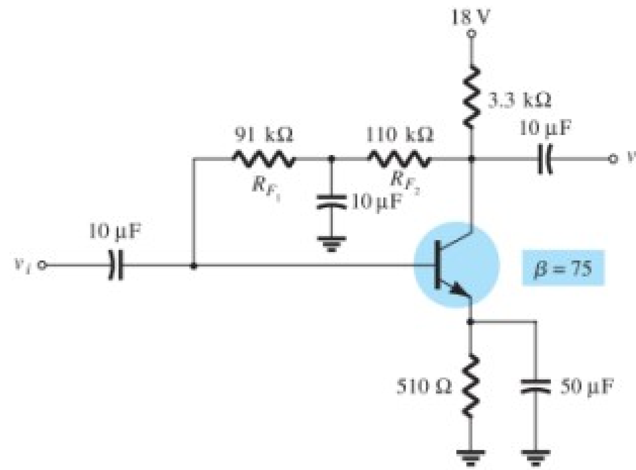
$$I_{C_{sat}} = I_{C_{max}} = \frac{V_{CC}}{R_C + R_E}$$

- Load-Line Analysis

Continuing with the approximation $I'_C = I_C$ results in the same load line defined for the voltage-divider and emitter-biased configurations.

The level of I_{BQ} is defined by the chosen bias configuration.

EXAMPLE 4.14 Determine the dc level of I_B and V_C for the network of Fig. 4.42.



Solution: In this case, the base resistance for the dc analysis is composed of two resistors with a capacitor connected from their junction to ground. For the dc mode, the capacitor assumes the open-circuit equivalence, and $R_B = R_{F_1} + R_{F_2}$.

Solving for I_B gives

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + \beta(R_C + R_E)}$$

$$= \frac{18\text{ V} - 0.7\text{ V}}{(91\text{ k}\Omega + 110\text{ k}\Omega) + (75)(3.3\text{ k}\Omega + 0.51\text{ k}\Omega)}$$

$$= \frac{17.3\text{ V}}{201\text{ k}\Omega + 285.75\text{ k}\Omega} = \frac{17.3\text{ V}}{486.75\text{ k}\Omega}$$

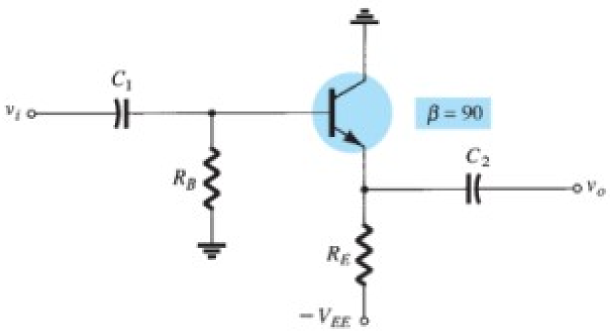
$$= \mathbf{35.5\ \mu A}$$

$$I_C = \beta I_B$$
$$= (75)(35.5\ \mu\text{A})$$
$$= 2.66\text{ mA}$$

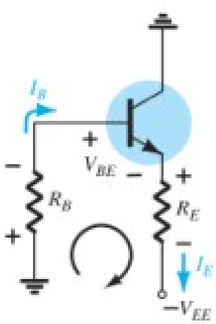
$$V_C = V_{CC} - I'_C R_C \cong V_{CC} - I_C R_C$$
$$= 18\text{ V} - (2.66\text{ mA})(3.3\text{ k}\Omega)$$
$$= 18\text{ V} - 8.78\text{ V}$$
$$= \mathbf{9.22\ V}$$

Emitter-Follower Configuration

- Common-collecter (emitter-follower) configuration.



- dc equivalent ct



i/p ct

$$-I_B R_B - V_{BE} - I_E R_E + V_{EE} = 0$$

$$I_B R_B + (\beta + 1) I_B R_E = V_{EE} - V_{BE}$$

$$\boxed{I_B = \frac{V_{EE} - V_{BE}}{R_B + (\beta + 1) R_E}}$$

o/p ct

$$-V_{CE} - I_E R_E + V_{EE} = 0$$

$$\boxed{V_{CE} = V_{EE} - I_E R_E}$$

EXAMPLE 4.16 Determine V_{CE_Q} and I_{E_Q} for the network of Fig. 4.48.

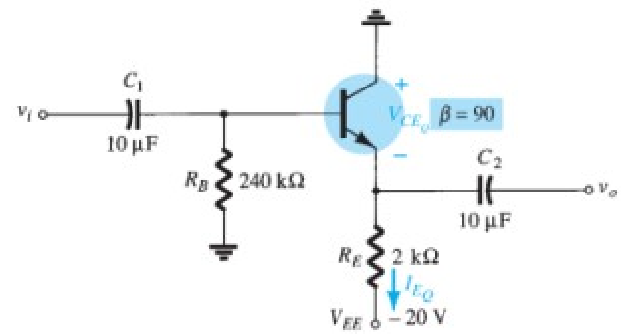


FIG. 4.48
Example 4.16.

Solution:

Eq. 4.44:

$$I_B = \frac{V_{EE} - V_{BE}}{R_B + (\beta + 1)R_E}$$

$$= \frac{20\text{ V} - 0.7\text{ V}}{240\text{ k}\Omega + (90 + 1)2\text{ k}\Omega} = \frac{19.3\text{ V}}{240\text{ k}\Omega + 182\text{ k}\Omega}$$

$$= \frac{19.3\text{ V}}{422\text{ k}\Omega} = 45.73\ \mu\text{A}$$

and Eq. 4.45:

$$V_{CE_Q} = V_{EE} - I_E R_E$$

$$= V_{EE} - (\beta + 1) I_B R_E$$

$$= 20\text{ V} - (90 + 1)(45.73\ \mu\text{A})(2\text{ k}\Omega)$$

$$= 20\text{ V} - 8.32\text{ V}$$

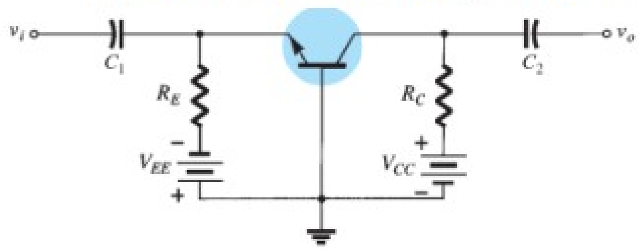
$$= \mathbf{11.68\ V}$$

$$I_{E_Q} = (\beta + 1) I_B = (91)(45.73\ \mu\text{A})$$

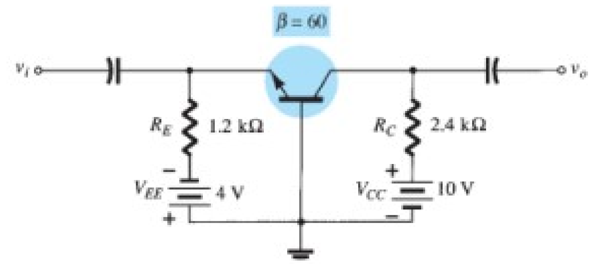
$$= 4.16\text{ mA}$$

Common-Base Configuration

- Common-base configuration



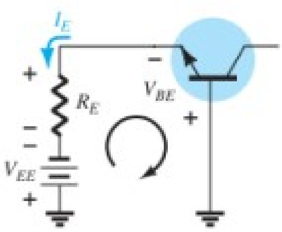
EXAMPLE 4.17 Determine the currents I_E and I_B and the voltages V_{CE} and V_{CB} for the common-base configuration of Fig. 4.52.



- i/p ct

$$-V_{EE} + I_E R_E + V_{BE} = 0$$

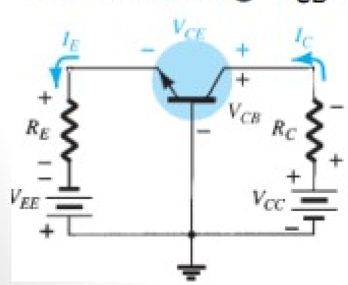
$$\boxed{I_E = \frac{V_{EE} - V_{BE}}{R_E}}$$



$$-V_{EE} + I_E R_E + V_{CE} + I_C R_C - V_{CC} = 0$$
$$V_{CE} = V_{EE} + V_{CC} - I_E R_E - I_C R_C$$
$$I_E \cong I_C$$

$$\boxed{V_{CE} = V_{EE} + V_{CC} - I_E(R_C + R_E)}$$

- Determining V_{CB} & V_{CE}



$$V_{CB} + I_C R_C - V_{CC} = 0$$
$$V_{CB} = V_{CC} - I_C R_C$$
$$I_C \cong I_E$$

$$\boxed{V_{CB} = V_{CC} - I_C R_C}$$

Solution: Eq. 4.46:

$$I_E = \frac{V_{EE} - V_{BE}}{R_E} = \frac{4\text{ V} - 0.7\text{ V}}{1.2\text{ k}\Omega} = \mathbf{2.75\text{ mA}}$$

$$I_B = \frac{I_E}{\beta + 1} = \frac{2.75\text{ mA}}{60 + 1} = \frac{2.75\text{ mA}}{61} = \mathbf{45.08\ \mu A}$$

Eq. 4.47:

$$\begin{aligned} V_{CE} &= V_{EE} + V_{CC} - I_E(R_C + R_E) \\ &= 4\text{ V} + 10\text{ V} - (2.75\text{ mA})(2.4\text{ k}\Omega + 1.2\text{ k}\Omega) \\ &= 14\text{ V} - (2.75\text{ mA})(3.6\text{ k}\Omega) \\ &= 14\text{ V} - 9.9\text{ V} \\ &= \mathbf{4.1\text{ V}} \end{aligned}$$

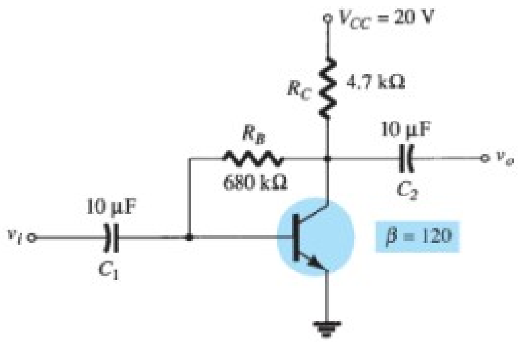
Eq. 4.48:

$$\begin{aligned} V_{CB} &= V_{CC} - I_C R_C = V_{CC} - \beta I_B R_C \\ &= 10\text{ V} - (60)(45.08\ \mu\text{A})(24\text{ k}\Omega) \\ &= 10\text{ V} - 6.49\text{ V} \\ &= \mathbf{3.51\text{ V}} \end{aligned}$$

MISCELLANEOUS BIAS CONFIGURATIONS

EXAMPLE 4.18 For the network of Fig. 4.53:

a. Determine I_{C_Q} and V_{CE_Q}.
b. Find V_B, V_C, V_E, and V_{BC}.



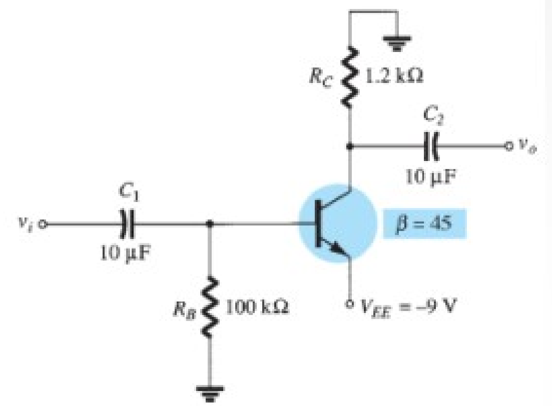
Solution:

a. The absence of R_E reduces the reflection of resistive levels to simply that of R_C, and the equation for I_B reduces to

$$I_B = \frac{V_{CC} - V_{BE}}{R_B + \beta R_C}$$
$$= \frac{20\text{ V} - 0.7\text{ V}}{680\text{ k}\Omega + (120)(4.7\text{ k}\Omega)} = \frac{19.3\text{ V}}{1.244\text{ M}\Omega}$$
$$= \mathbf{15.51\ \mu A}$$
$$I_{C_Q} = \beta I_B = (120)(15.51\ \mu\text{A})$$
$$= \mathbf{1.86\ mA}$$
$$V_{CE_Q} = V_{CC} - I_C R_C$$
$$= 20\text{ V} - (1.86\text{ mA})(4.7\text{ k}\Omega)$$
$$= \mathbf{11.26\ V}$$

b.
$$V_B = V_{BE} = \mathbf{0.7\ V}$$
$$V_C = V_{CE} = \mathbf{11.26\ V}$$
$$V_E = \mathbf{0\ V}$$
$$V_{BC} = V_B - V_C = 0.7\text{ V} - 11.26\text{ V}$$
$$= \mathbf{-10.56\ V}$$

EXAMPLE 4.19 Determine V_C and V_B for the network of Fig. 4.54.



Solution: Applying Kirchhoff's voltage law in the clockwise direction for the base–emitter loop results in

$$-I_B R_B - V_{BE} + V_{EE} = 0$$

and

$$I_B = \frac{V_{EE} - V_{BE}}{R_B}$$

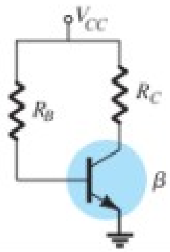
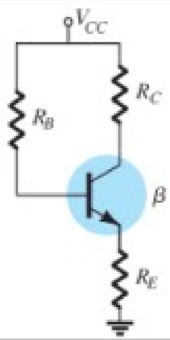
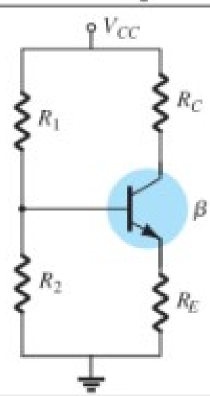
Substitution yields

$$I_B = \frac{9\text{ V} - 0.7\text{ V}}{100\text{ k}\Omega}$$
$$= \frac{8.3\text{ V}}{100\text{ k}\Omega}$$
$$= 83\ \mu\text{A}$$

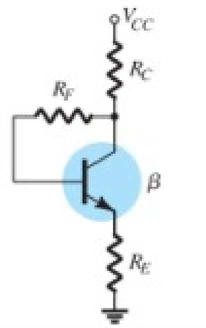
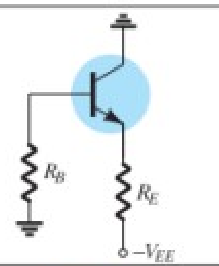
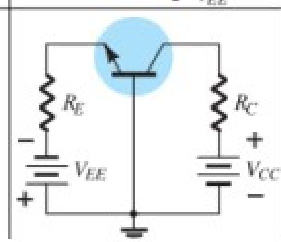
$$I_C = \beta I_B$$
$$= (45)(83\ \mu\text{A})$$
$$= 3.735\text{ mA}$$
$$V_C = -I_C R_C$$
$$= -(3.735\text{ mA})(1.2\text{ k}\Omega)$$
$$= \mathbf{-4.48\ V}$$
$$V_B = -I_B R_B$$
$$= -(83\ \mu\text{A})(100\text{ k}\Omega)$$
$$= \mathbf{-8.3\ V}$$

Summary Table

BJT Bias Configurations

Type	Configuration	Pertinent Equations
Fixed-bias		$I_B = \dfrac{V_{CC} - V_{BE}}{R_B}$ $I_C = \beta I_B, I_E = (\beta + 1)I_B$ $V_{CE} = V_{CC} - I_C R_C$
Emitter-bias		$I_B = \dfrac{V_{CC} - V_{BE}}{R_B + (\beta + 1)R_E}$ $I_C = \beta I_B, I_E = (\beta + 1)I_B$ $R_i = (\beta + 1)R_E$ $V_{CE} = V_{CC} - I_C(R_C + R_E)$
Voltage-divider bias		EXACT: $R_{Th} = R_1 \| R_2, E_{Th} = \dfrac{R_2 V_{CC}}{R_1 + R_2}$ $I_B = \dfrac{E_{Th} - V_{BE}}{R_{Th} + (\beta + 1)R_E}$ $I_C = \beta I_B, I_E = (\beta + 1)I_B$ $V_{CE} = V_{CC} - I_C(R_C + R_E)$ APPROXIMATE: $\beta R_E \geq 10R_2$ $V_B = \dfrac{R_2 V_{CC}}{R_1 + R_2}, V_E = V_B - V_{BE}$ $I_E = \dfrac{V_E}{R_E}, I_B = \dfrac{I_E}{\beta + 1}$ $V_{CE} = V_{CC} - I_C(R_C + R_E)$

Summary Table..

Collector-feedback		$I_B = \dfrac{V_{CC} - V_{BE}}{R_F + \beta(R_C + R_E)}$ $I_C = \beta I_B, I_E = (\beta + 1)I_B$ $V_{CE} = V_{CC} - I_C(R_C + R_E)$
Emitter-follower		$I_B = \dfrac{V_{EE} - V_{BE}}{R_B + (\beta + 1)R_E}$ $I_C = \beta I_B, I_E = (\beta + 1)I_B$ $V_{CE} = V_{EE} - I_E R_E$
Common-base		$I_E = \dfrac{V_{EE} - V_{BE}}{R_E}$ $I_B = \dfrac{I_E}{\beta + 1}, I_C = \beta I_B$ $V_{CE} = V_{EE} + V_{CC} - I_E(R_C + R_E)$ $V_{CB} = V_{CC} - I_C R_C$