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Applying Bernoulli's eqn b/w A and D.

$$\underbrace{\frac{P_A}{\rho g} + \frac{V_A^2}{2g} + z_A}_{HA} = \underbrace{\left(\frac{P_D}{\rho g} + \frac{V_D^2}{2g} + z_D + h_{L_1} \right)}_{HD}$$

$$HA \neq HD + h_{L_1} \Rightarrow$$

$$HA = HD + \frac{.024 \times 1200 \times (.06)^2}{12 \times (.3)^5}$$

$$HD = 36.4 \text{ m.}$$

As the total head at B is greater than the total head at D. Therefore the flow is from B to D.

Applying Bernoulli's eqn b/w B and D.

$$HB = HD + h_{L_2}$$

$$38 = 36.4 + \frac{f_2 l_2 Q_2^2}{12 d_2^5}$$

$$38 = 36.4 + \frac{.024 \times 600 \times Q_2^2}{12 \times (.2)^5}$$

$$Q_2 = 0.02 \text{ m}^3/\text{s.} \stackrel{1}{=} 20 \text{ liters/s.}$$

from continuity eqn

$$Q_1 + Q_2 = Q_3$$

$$60 + 20 = Q_3 = 80 \text{ liters/s.}$$

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Apply Bernoulli's eqn between B & D.

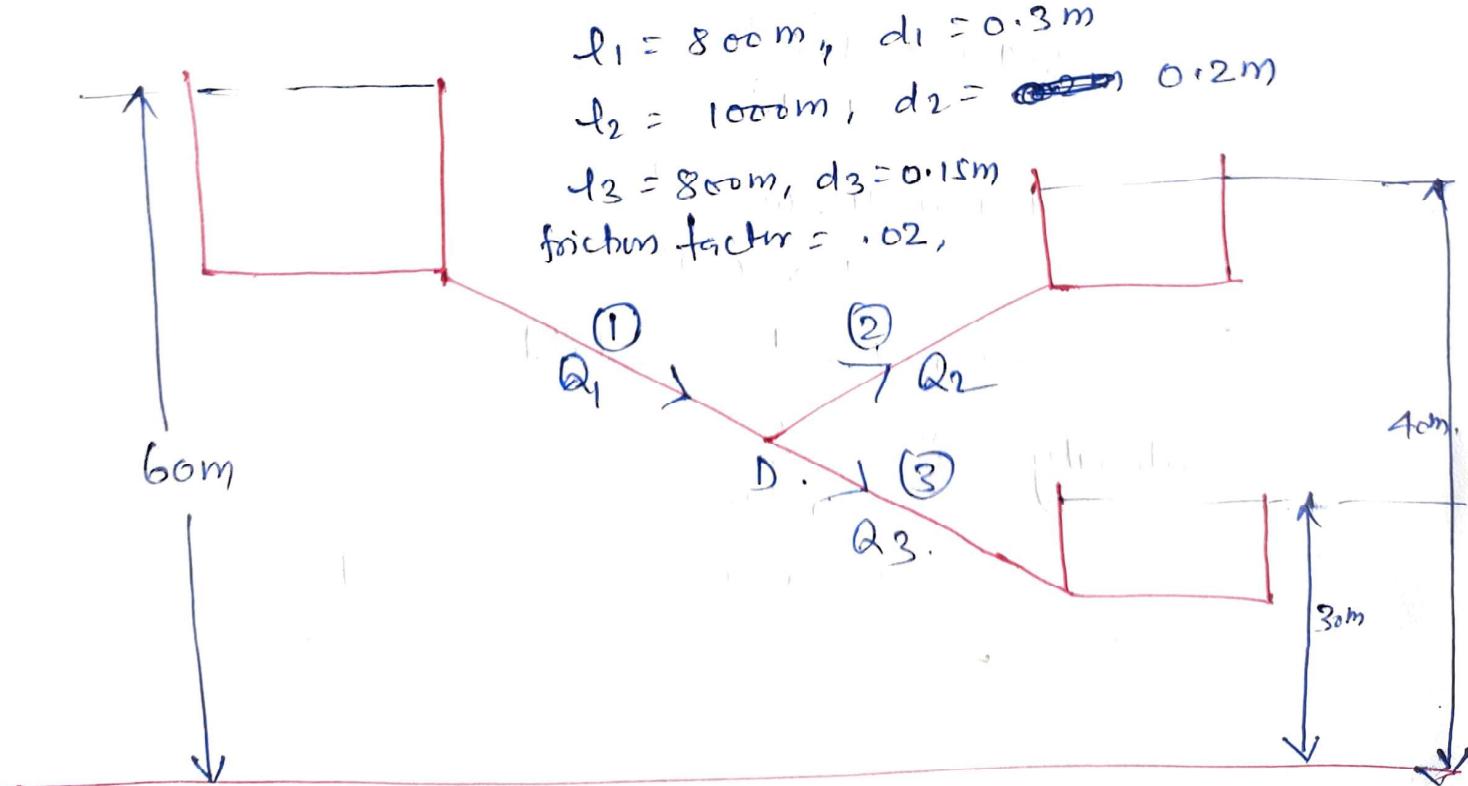
$$H_D = H_C + h_{L3}$$

$$36.4 = H_C + \frac{f l_3 Q_3^2}{\tau_2 \times d_3^5}$$

$$36.4 = H_C + \frac{0.024 \times 800 \times (0.08)^2}{12 \times (0.3)^5}$$

$H_C = 32.2 \text{ m.}$

Q:- Three reservoirs A, B and C are connected by a pipe system as shown in fig. along with direction. Determine the total head at junction D.

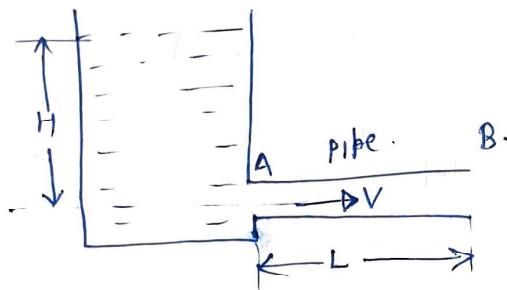


Power transmission through pipe.

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The transmission of power through pipes carrying water or other liquids is commonly used for working of several hydraulic machines. The hydraulic power transmitted by a pipe however depends on.

- The discharge passing through the pipe.
- The total head of water.



weight of water flowing through the pipe per second :-

$$\frac{s}{v} = \dot{m} \cdot g = s \cdot A \cdot v \cdot g = wAV.$$

$$m = s \times \text{volume}$$

$\frac{s}{v} \times A \times L = sVv$ head available at B. (neglecting minor loss)

$$= H - h_f = H - \frac{4f LV^2}{2g \cdot d}$$

$$\eta = \frac{H - h_f}{H}$$

efficiency of transmission

power required to overcome the frictional loss.

$$P = \sigma g Q h_f \quad \text{head loss due to friction.}$$

$$\text{power available} = \sigma g Q H.$$

power available at the outlet of the pipe.

$$P = \sigma g Q (H - h_f)$$

$$P = \sigma g \times A V (H - h_f)$$

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Condition for maximum power transmission

$$P = \omega \cdot A \left[H \cdot V - \frac{4 f L V^2}{2 g d} \right]$$

$$P = f(V) \dots$$

$$\frac{dP}{dV} = 0 \quad , \quad \frac{dP}{dV} = g \times \frac{\pi}{4} \cdot d^2 \cdot \frac{d}{dV} \left[H \cdot V - \frac{4 f L V^2}{2 g d} \right] = 0$$

~~$$\Rightarrow H - \frac{4 f L V^2}{2 g d} = 0$$~~

$$H - 3 \frac{4 f L V^2}{2 g d} = 0$$

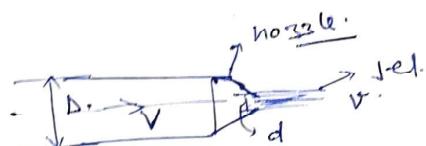
$$H - 3 h_f = 0 \Rightarrow H = 3 h_f$$

$$h_f = \frac{H}{3}$$

Condition for max^m power.

$$\eta = \frac{H - h_f}{H} = \frac{H - \frac{H}{3}}{H} = \frac{2}{3} = 66.7\%$$

Flow through nozzle at the end of a pipe! -



D → pipe diameter, L → Length of pipe, V → velocity of flow in pipe

H → head available [height of water level in the reservoir above the centre-line of the nozzle]

f → co-efficient of friction for the pipe.

v → velocity of flow at the outlet of nozzle.

Head loss due to friction in pipe

$$h_f = \frac{4 f L V^2}{2 \times g \times D}$$

available head at the base of nozzle.

$$= H - \frac{4 f L V^2}{2 \times g \times D}$$

losses in the nozzle is neglected.

$$\text{Total head at the nozzle outlet} = \frac{V^2}{2g}$$

$$H = h_f + \frac{V^2}{2g}$$

from continuity eqn. $A_1 V_1 = A_2 V_2$

$$V_2 = \frac{A_1 V_1}{A_2}$$

$$H = \frac{4fL}{2g} \frac{V^2}{D} + \frac{V^2}{2g} \Rightarrow \frac{4fL}{D} \frac{q^2 v^2}{2g A^2} + \frac{V^2}{2g}$$

$$= \frac{V^2}{2g} \left[1 + \frac{4fL q^2}{D A^2} \right] \Rightarrow V = \sqrt{\frac{2g H}{1 + \frac{4fL q^2}{D A^2}}}$$

discharge through the nozzle - $q \cdot V$.

Power transmitted through the nozzle :-

$$\dot{m} = S \cdot q \cdot V \text{ kg/s.}$$

$$\begin{aligned} \text{K.E. of jet at outlet of nozzle} \\ = \frac{1}{2} \dot{m} \cdot V^2 = \frac{1}{2} \times S \cdot q \cdot V \times V^2 = \frac{1}{2} S \cdot q \cdot V^3. \end{aligned}$$

Power available at the outlet of nozzle :-

$$= \frac{1}{2} S \cdot q \cdot V^3 \text{ watt.}$$

Power available at the inlet of pipe = $Sg Q H$.

eff. of power transmission through the nozzle.

$$\eta = \frac{\frac{1}{2} S \cdot q \cdot V^3}{Sg Q H} = \frac{V^2}{2g H} = \frac{1}{1 + \frac{4fL q^2}{D A^2}}$$