Magnetic Fields

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Biot Savart's Law

It states that the differential magnetic field intensity dH produced at a point P, by the differential current element IdI is proportional to the product IdI and the sine of the angle α between the element and the line joining the P to the element and is inversely proportional to the square of the distance R between P and the element,

That is,

 $dH \propto \frac{I \, dl \, \sin \alpha}{R^2}$

$$dH = \frac{kI\,dl\,\sin\alpha}{R^2}$$



where k is the constant of proportionality. In SI units, $k = 1/4\pi$, so

$$dH = \frac{I\,dl\,\sin\alpha}{4\pi R^2}$$

or

Biot Savart's Law

• Vector form

$$d\mathbf{H} = \frac{I\,d\mathbf{I} \times \mathbf{a}_R}{4\pi R^2} = \frac{I\,d\mathbf{I} \times \mathbf{R}}{4\pi R^3}$$

• For differential current distribution

$$\mathbf{H} = \int_{L} \frac{I \, d\mathbf{l} \times \mathbf{a}_{R}}{4\pi R^{2}} \quad \text{(line current)}$$
$$\mathbf{H} = \int_{S} \frac{\mathbf{K} \, dS \times \mathbf{a}_{R}}{4\pi R^{2}} \quad \text{(surface current)}$$
$$\mathbf{H} = \int_{v} \frac{\mathbf{J} \, dv \times \mathbf{a}_{R}}{4\pi R^{2}} \quad \text{(volume current)}$$

Field due to straight current carrying filamentary conductor of finite length

- We assume that the conductor is along z axis with its upper and lower ends respectively, subtending angle α1 and α2 at P, the pont at which H is to be determined.
- If we consider the contribution **dH** at P due to an element dl at (0,0,z)

$$d\mathbf{H} = \frac{I\,d\mathbf{I}\times\mathbf{R}}{4\pi R^3}$$

But $d\mathbf{l} = dz \, \mathbf{a}_z$ and $\mathbf{R} = \rho \mathbf{a}_\rho - z \mathbf{a}_z$, so

$$d\mathbf{l} \times \mathbf{R} = \rho \, dz \, \mathbf{a}_{\phi}$$

Hence,

$$\mathbf{H} = \int \frac{I\rho \, dz}{4\pi [\rho^2 + z^2]^{3/2}} \, \mathbf{a}_{\phi}$$



Field due to straight current carrying filamentary conductor of finite length

Letting $z = \rho \cot \alpha$, $dz = -\rho \operatorname{cosec}^2 \alpha \, d\alpha$, and eq. (7.11) becomes

 $\mathbf{H} = -\frac{1}{4\pi} \int_{\alpha_1}^{\alpha_2} \frac{\rho^2 \operatorname{cosec}^2 \alpha \, d\alpha}{\rho^3 \operatorname{cosec}^3 \alpha} \, \mathbf{a}_{\phi}$ $= -\frac{I}{4\pi\rho} \, \mathbf{a}_{\phi} \int_{\alpha_1}^{\alpha_2} \sin \alpha \, d\alpha$

or

$$\mathbf{H} = \frac{I}{4\pi\rho} \left(\cos\alpha_2 - \cos\alpha_1\right) \mathbf{a}_{\phi}$$

Semiinfinite $\alpha 1=90$ and $\alpha 2=0$

$$\mathbf{H} = \frac{I}{4\pi\rho} \, \mathbf{a}_{\phi}$$

Field due to straight current carrying filamentary conductor of finite length

Infinite $\alpha 1=180$ and $\alpha 2=0$

$$\mathbf{H} = \frac{I}{2\pi\rho} \, \mathbf{a}_{\phi}$$

Numerical 1

carries a current of 10 A. Find H at (0, 0, 5)

The conducting triangular loop in Figure ' due to side 1 of the loop.





Numerical 2

A circular loop located on $x^2 + y^2 = 9$, z = 0 carries a direct current of 10 A along \mathbf{a}_{ϕ} . Determine **H** at (0, 0, 4) and (0, 0, -4).



$$d\mathbf{H} = \frac{I\,d\mathbf{I} \times \mathbf{R}}{4\pi R^3}$$

where $d\mathbf{l} = \rho \, d\phi \, \mathbf{a}_{\phi}, \mathbf{R} = (0, 0, h) - (x, y, 0) = -\rho \mathbf{a}_{\rho} + h \mathbf{a}_{z}$, and

$$d\mathbf{l} \times \mathbf{R} = \begin{vmatrix} \mathbf{a}_{\rho} & \mathbf{a}_{\phi} & \mathbf{a}_{z} \\ 0 & \rho \, d\phi & 0 \\ -\rho & 0 & h \end{vmatrix} = \rho h \, d\phi \, \mathbf{a}_{\rho} + \rho^{2} \, d\phi \, \mathbf{a}_{z}$$

Hence,

$$d\mathbf{H} = \frac{I}{4\pi[\rho^2 + h^2]^{3/2}} \left(\rho h \, d\phi \, \mathbf{a}_{\rho} + \rho^2 \, d\phi \, \mathbf{a}_z\right) = dH_{\rho} \, \mathbf{a}_{\rho} + dH_z \, \mathbf{a}_z$$

• Due to symmetry , radial components are cancelled out in pair, only z component are summed up

$$\mathbf{H} = \int dH_z \, \mathbf{a}_z = \int_0^{2\pi} \frac{I\rho^2 \, d\phi \, \mathbf{a}_z}{4\pi [\rho^2 + h^2]^{3/2}} = \frac{I\rho^2 2\pi \mathbf{a}_z}{4\pi [\rho^2 + h^2]^{3/2}}$$

$$\mathbf{H} = \frac{l\rho^2 \mathbf{a}_z}{2[\rho^2 + h^2]^{3/2}}$$

(a) Substituting I = 10 A, $\rho = 3$, h = 4 gives

$$\mathbf{H}(0, 0, 4) = \frac{10 (3)^2 \mathbf{a}_z}{2[9 + 16]^{3/2}} = 0.36\mathbf{a}_z \,\mathrm{A/m}$$

(b) Notice from $d\mathbf{l} \times \mathbf{R}$ above that if *h* is replaced by -h, the *z*-component of $d\mathbf{H}$ remains the same while the ρ -component still adds up to zero due to the axial symmetry of the loop. Hence

$$\mathbf{H}(0, 0, -4) = \mathbf{H}(0, 0, 4) = 0.36\mathbf{a}_z \,\mathrm{A/m}$$

Numerical 3

A solenoid of length ℓ and radius *a* consists of *N* turns of wire carrying current *I*. Show that at point *P* along its axis,

$$\mathbf{H} = \frac{nI}{2} \left(\cos \theta_2 - \cos \theta_1 \right) \mathbf{a}_z$$

where $n = N/\ell$, θ_1 and θ_2 are the angles subtended at *P* by the end turns as illustrated in Figure Also show that if $\ell \gg a$, at the center of the solenoid,

$$\mathbf{H} = nI\mathbf{a}_z$$



Consider the cross section of the solenoid in Fig. Since the solenoid consist of a circular loop.The contribution to the magnetic field H at P by an element of the of the solenoid of length dz is

$$dH_z = \frac{I \, dl \, a^2}{2[a^2 + z^2]^{3/2}} = \frac{I a^2 n \, dz}{2[a^2 + z^2]^{3/2}}$$

where $dl = n dz = (N/\ell) dz$. From Figure 7.9, $\tan \theta = a/z$; that is,

$$dz = -a \operatorname{cosec}^2 \theta \, d\theta = -\frac{[z^2 + a^2]^{3/2}}{a^2} \sin \theta \, d\theta$$

Hence,

$$dH_z = -\frac{nI}{2}\sin\theta \ d\theta$$

or

$$H_z = -\frac{nI}{2} \int_{\theta_1}^{\theta_2} \sin \theta \, d\theta$$

Thus

$$\mathbf{H} = \frac{nI}{2} \left(\cos \theta_2 - \cos \theta_1 \right) \mathbf{a}_z$$

as required. Substituting $n = N/\ell$ gives

$$\mathbf{H} = \frac{NI}{2\ell} \left(\cos \theta_2 - \cos \theta_1\right) \mathbf{a}_z$$

At the center of the solenoid,

$$\cos \theta_2 = \frac{\ell/2}{\left[a^2 + \ell^2/4\right]^{1/2}} = -\cos \theta_1$$

and

$$\mathbf{H} = \frac{In\ell}{2[a^2 + \ell^2/4]^{1/2}} \,\mathbf{a}_z$$

If
$$\ell \gg a$$
 or $\theta_2 \simeq 0^\circ$, $\theta_1 \simeq 180^\circ$,

$$\mathbf{H} = nI\mathbf{a}_z = \frac{NI}{\ell}\,\mathbf{a}_z$$